

RESEARCH ARTICLE



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## DUAL BAND BODY ANTENNA FOR C BAND APPLICATIONS

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### ABSTRACT

This paper presents design of body phased array using optimized dual frequency body patch antenna for C band focusing on 5 and 6 GHz frequency band. Inclusion of slots with near about symmetrical distribution on conducting plane and notches in both plane and defected ground structure and also changing feed position for impedance matching. Return loss of final design is -10.14 dB for 5.2 GHz frequency and VSWR of 1.89 and -15.49dB and VSWR of 1.54 for 6.4 GHz frequency. Proposed antenna gives dual band operation and shows good bandwidth and simulated results for two frequency bands.

**Key Words** — Body antenna, Patch, slot, DGS, feedline, notch, Body Area Network

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### INTRODUCTION

C band body radars work on a wavelength of 4-6 cm and a frequency of 4-6 GHz. Because of the wavelength and frequency, the antenna size does not require being very large. This makes C band radars compatible for body area network. Signal is easily attenuated; C band radar is best used for short range body signal observation. The frequency allows C band radars to generate a smaller beam width using a smaller body antenna. It not require more power compare the S band radar [1,2,11].

Body wireless communication requires many antennas to be worked together for scanning, tracking and other such needs for precision. Combination of more than one antenna can be called as array. The radiation pattern of a single element is relatively wide, low values of directivity (gain). So it is

compulsory to design antennas with very high gains for long distance communication. This can possible by increasing the electrical size of the antenna. Enlarging the dimensions of single elements always leads to more directive characteristics. Next way to enlarge the dimensions of the antenna, without increasing the size of the single elements, is to make an assembly of radiating elements in a geometrical and electrical configuration. This new antenna, formed by multi-elements, is called to as an array. Generally the elements of an array are identical. But it is often convenient, simpler, and more practical. The single elements of an array may be of any form (wires, apertures, etc.) that we shift a baseband information signal to a frequency or frequencies suitable for electromagnetic propagation to the desired destination. Apart from that when we

actually radiate energy in free space there are chances of mixing noise and also change in polarization resulting in undesired effects. This can be avoided by introduction of phase changes between each element of array. In other words by using phase changes at each element overall performance can be improved. Thus a concept of phased array helps in transmission and reception of signals. Phase changes can be introduced by numerous methods it can be by much different planar structure [7, 8, 9, 10].

**DESIGN**

Width=30.6mm and length= 27.40mm .

Here modification is done in two different plane i.e. on top plane and ground plane separately. For top plane four square slots of size 5mm x 5mm are made on upper portion of the rectangular patch antenna. Ground plane is made defected. Regular defected structure is introduced in ground plane.

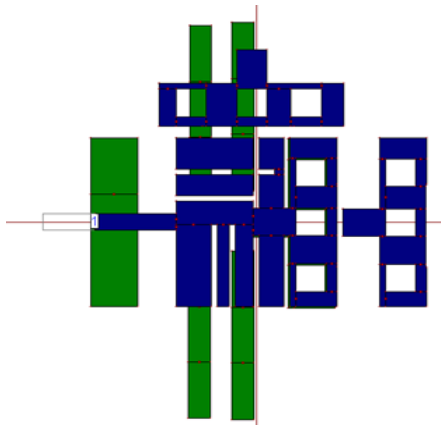


Fig. 1. Detail simulation window showing different dimensions of top conducting plane.

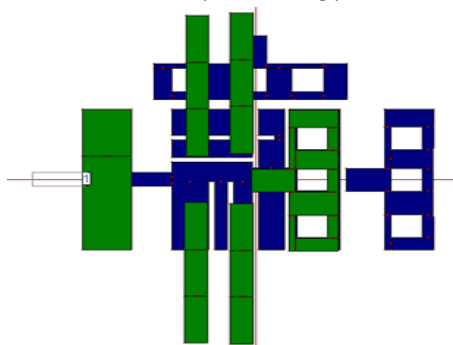


Fig. 2. Simulation window of defected ground structure for the proposed antenna

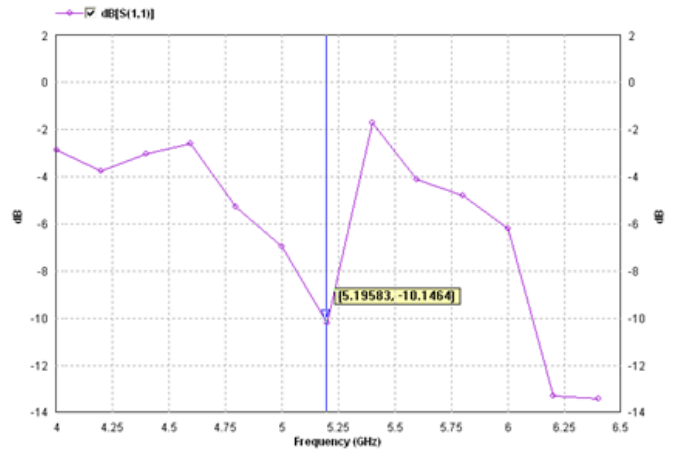


Fig. 3. Simulation of return loss for proposed antenna for 5.2 GHz

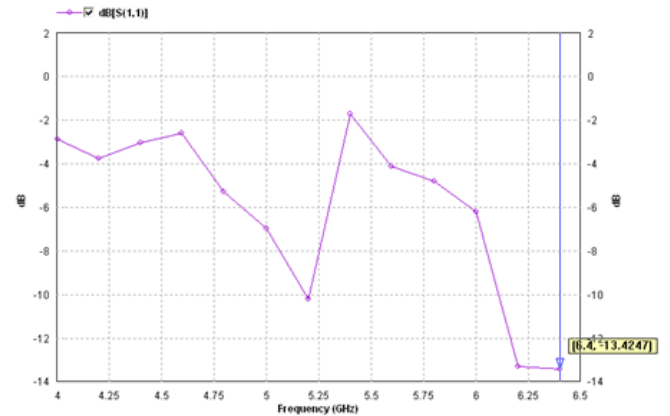


Fig. 4. Simulation of return loss for proposed antenna for 6.4 GHz

Return loss at 5.2 and 6.4 GHz was found to be -10.14dB and -13.42dB respectively.

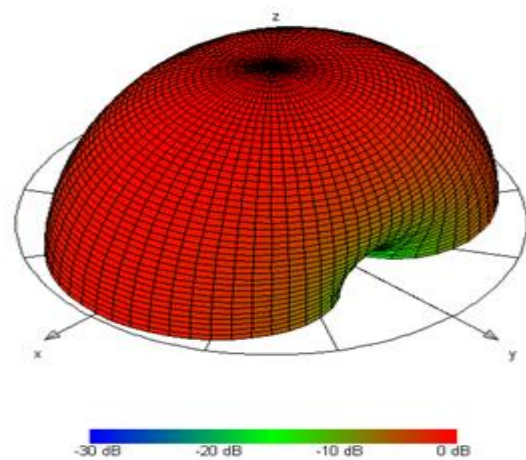


Fig. 5. Radiation pattern of antenna

The path that slots are used into the patch increases the resonant frequencies due to the change in the mean current paths of any resonant frequency (a mode). Dimension changing of a slot generate changes in the effective current way of a certain mode which in turn a shift in the resonant frequency. So the radiated fields are generated by the currents passes to the radiating edges of the patch, then vertical slots put close to these edges can handle the resonance frequency bands. Horizontal slots can be used to divide the patch into subsections which act as switches. These switches force the currents to travel through many ways according to the positions of the slots causing the antenna to resonant at different frequencies. The effect of the structure of the ground plane on the antenna performance is also controlled by mounting the proposed body antenna structure on either one of two different types of ground planes, the first is a conventional perfect electrical conductor (PEC) ground plane and the other is a defected ground structure (DGS). The DGS plane contain of an etched U shape. There advantages associated with using DGS planes. First, structures provide wider bandwidths with high gain and higher radiation efficiency. Second, these structures forbid the propagation of electromagnetic waves in a certain frequency band. Therefore, they can be used to block surface waves that usually corrupt antenna performance at a certain frequency band [4,10].

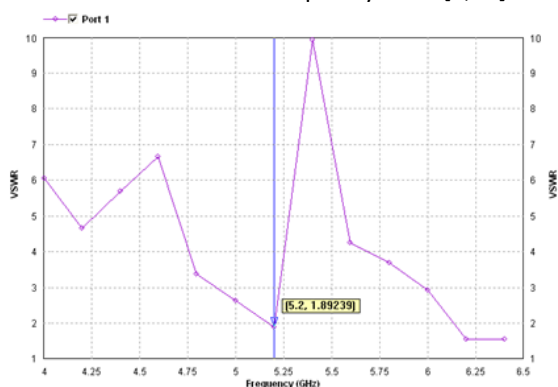


Fig. 6. Simulated VSWR of proposed patch antenna at 5.2 GHz

Bandwidth of first band was 1.28 GHz starting from 4.6GHz to 5.88 GHz. Similarly for second band bandwidth was 1.19 GHz starting with 7.29 GHz to 8.48GHz. More than 1 GHz bandwidth for two bands was achieved implying wideband applications.

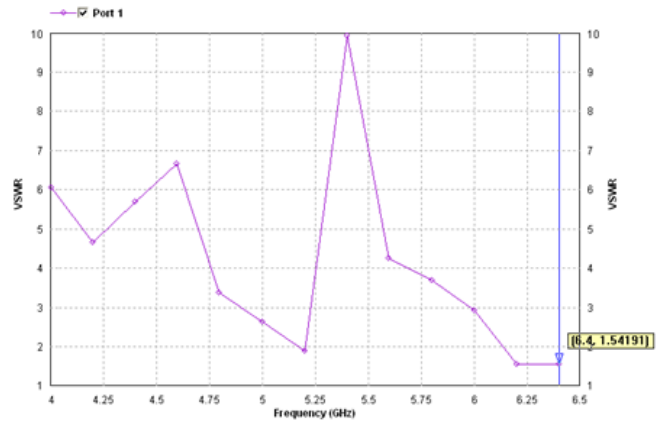


Fig. 7 Simulated VSWR of proposed patch antenna at 6.4 GHz

#### MEASUREMENT RESULTS

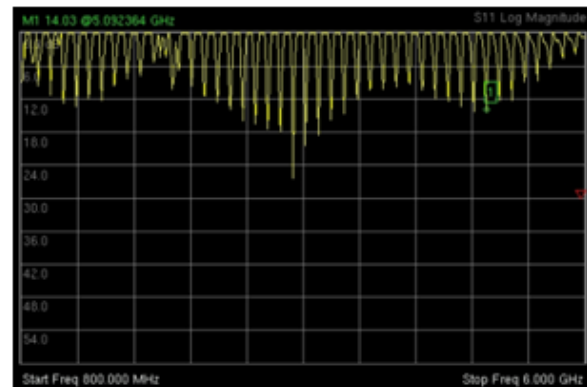


Fig. 8 Measured return loss at input port for 5.2 GHz antenna

Return loss was found to be -14.03dB at 5.2 GHz. Here there is improvement in measured result as compare to simulation.

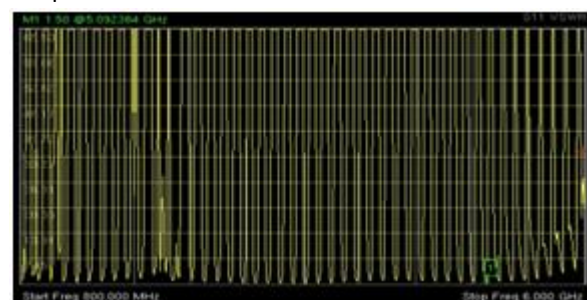


Fig. 9 Measured VSWR for 5.2 GHz antenna

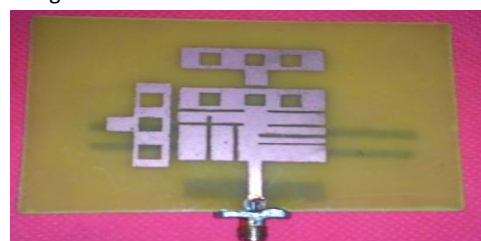


Fig. 10 Photograph for fabricated proposed antenna



Fig. 11 Photograph for fabricated proposed antenna

#### CONCLUSION

Modified design of patch antenna with defected ground structure (DGS) and slots on conducting plane provides simulation results having return loss of -10.14 dB and VSWR of 1.89 for 5.2 GHz while -13.42 dB return loss and 1.54 VSWR value for 6.4 GHz frequency range. Measured return loss is -14.03 dB and VSWR of 1.50 for 5.2 GHz.

#### ACKNOWLEDGEMENT

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